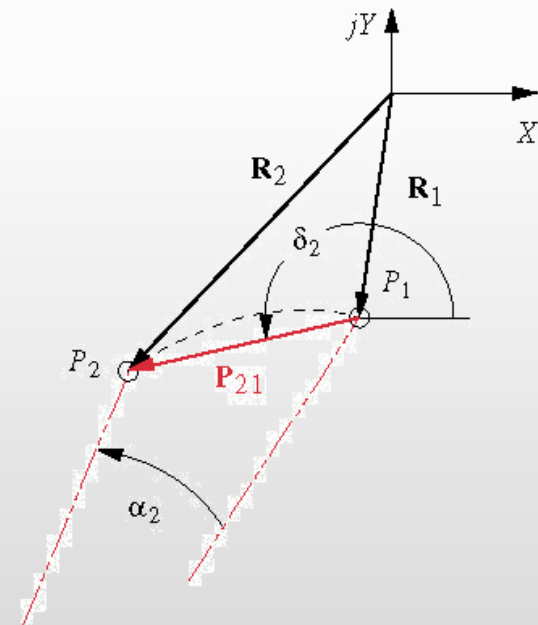
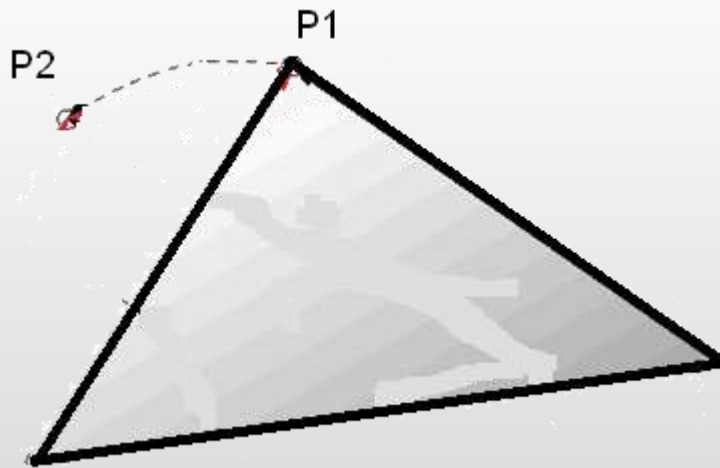


# Kinematics & Dynamics of Linkages

## Lecture 12: 2 Positions Analytical Synthesis

# 2-Position Motion Generation

- Design four bar linkage that will move a line on its coupler link such that a point  $P$  on that line will be first at  $P_1$  and later at  $P_2$  and will also rotate the line through an angle  $\alpha_2$

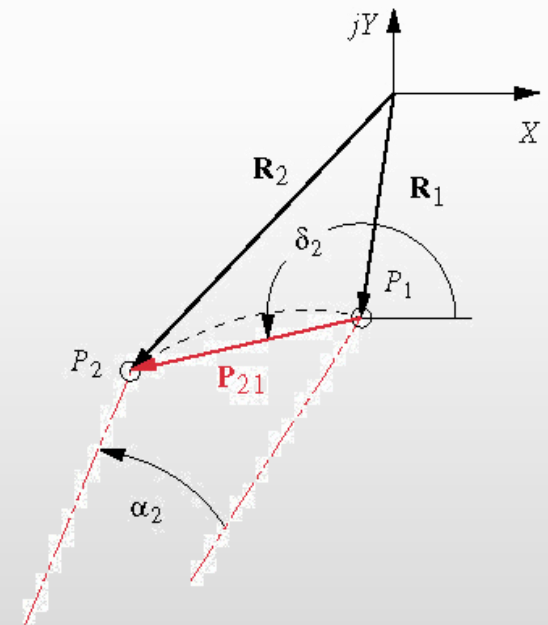




# 2-Position Procedure

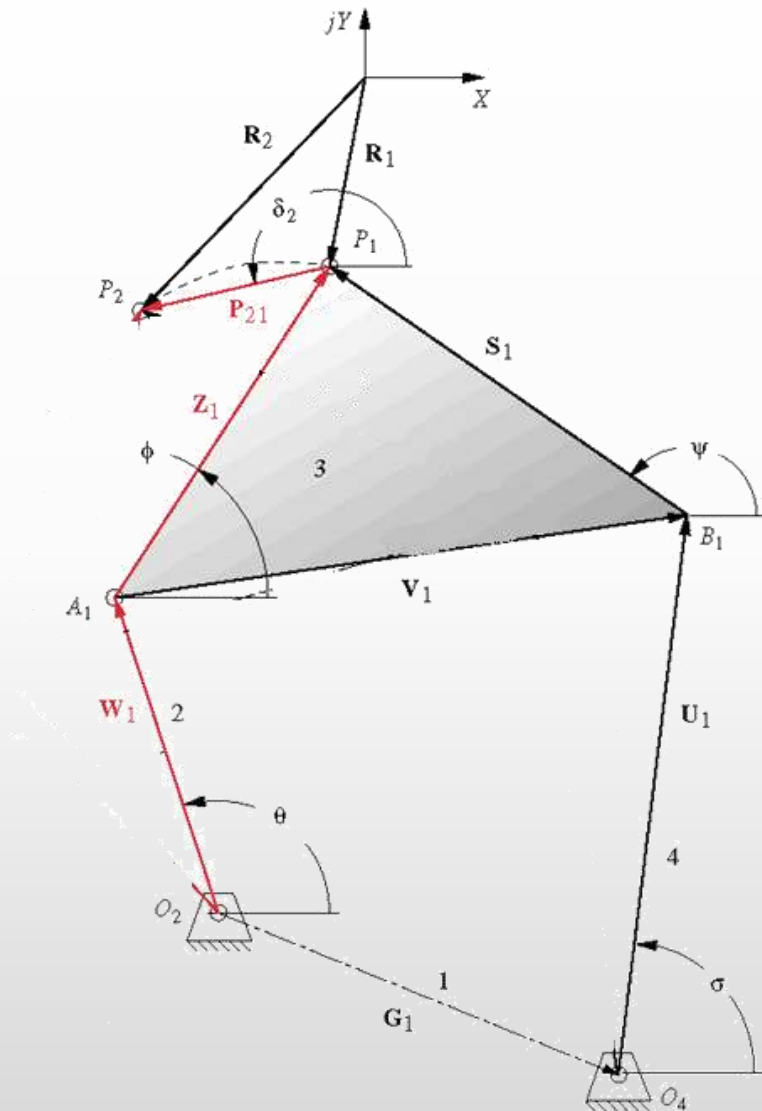
Define the 2 desired precision positions w/r to a chosen GCS

1. Use position vectors  $R_1$  and  $R_2$
2.  $\alpha_2$  is the change in orientation of link  $z$
3.  $p_{21}$  defines the distance from point  $P_1$  to  $P_2$
4.  $p_{21} = R_2 - R_1$



# 2-Position Procedure

- The dyad  $\mathbf{W}_1\mathbf{Z}_1$  defines the left half of the linkage. The dyad  $\mathbf{U}_1\mathbf{S}_1$  defines the right half of the linkage.
- Solve for the left side of the linkage (vectors  $\mathbf{W}_1, \mathbf{Z}_1$ ) and later use the same procedure to solve for the right side (vectors  $\mathbf{U}_1, \mathbf{S}_1$ ).



# 2-Position Procedure - Dyad 1

## 1<sup>st</sup> dyad: WZ

Define the following variables:

$w$  = length link2

$\theta$  = angle of link2 in first position

$\beta_2$  = change in angle of input link

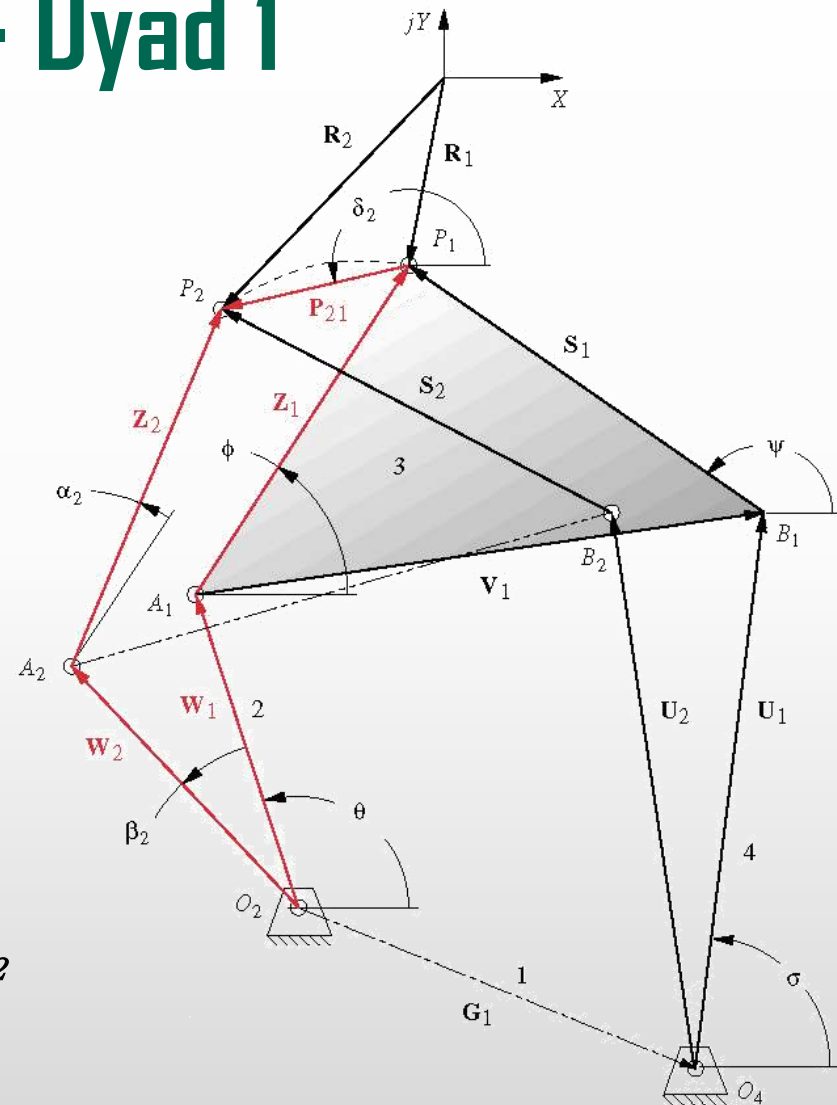
$z$  = distance from  $A$  and  $P$

$\Phi$  = orientation angle of  $L_3$  at position 1

$\alpha_2$  = change in orientation of link  $z$

$p_{21}$  = distance from point  $P_1$  to  $P_2$

$\delta_2$  = orientation angle of line from  $P_1$  to  $P_2$



# 2-Position Procedure – Dyad 1

## Equation of the 1<sup>st</sup> dyad

$$W_2 + Z_2 - P_{21} - Z_1 - W_1 = 0$$

$$w e^{j(\theta+\beta_2)} + z e^{j(\Phi+\alpha_2)} - p_{21} e^{j\delta_2} - z e^{j\Phi} - w e^{j\theta} = 0$$

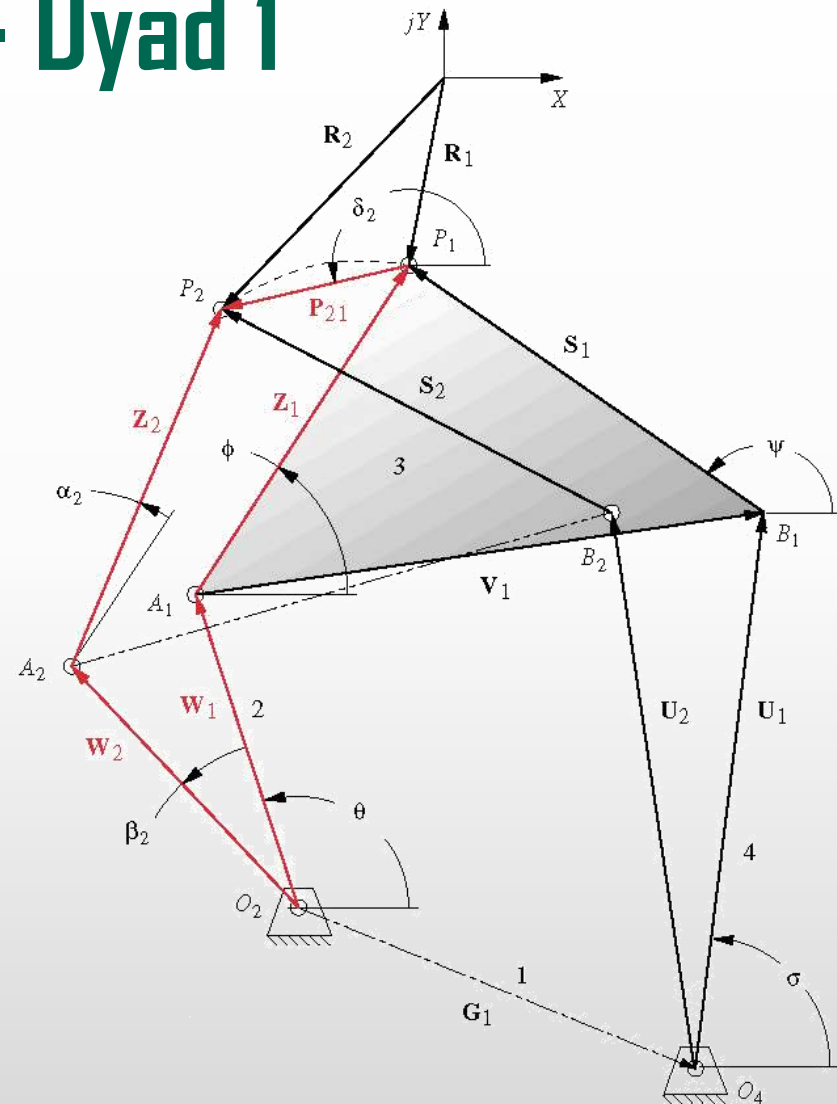
$$w e^{j\theta} (e^{j\beta_2} - 1) + z e^{j\Phi} (e^{j\alpha_2} - 1) = p_{21} e^{j\delta_2}$$

## Real part:

$$w \cos\theta (\cos\beta_2 - 1) - w \sin\theta \sin\beta_2 + z \cos\Phi (\cos\alpha_2 - 1) - z \sin\Phi \sin\alpha_2 = p_{21} \cos\delta_2$$

## Imaginary part:

$$w \sin\theta (\cos\beta_2 - 1) + w \cos\theta \sin\beta_2 + z \sin\Phi (\cos\alpha_2 - 1) + z \cos\Phi \sin\alpha_2 = p_{21} \sin\delta_2$$



# 2-Position Procedure – Dyad 1

## 2 Equations:

- $w \cos \theta (\cos \beta_2 - 1) - w \sin \theta \sin \beta_2 + z \cos \Phi (\cos \alpha_2 - 1) - z \sin \Phi \sin \alpha_2 = p_{21} \cos \delta_2$
- $w \sin \theta (\cos \beta_2 - 1) + w \cos \theta \sin \beta_2 + z \sin \Phi (\cos \alpha_2 - 1) + z \cos \Phi \sin \alpha_2 = p_{21} \sin \delta_2$

## There are 8 variables in the equations:

$w, \theta, \beta_2, z, \Phi, \alpha_2, p_{21}, \delta_2$

3 are given:  $\alpha_2, p_{21}$  and  $\delta_2$

Choose 3 variables and solve for 2.

## 2 Cases to be considered:

Choose  $\theta, \beta_2$  and  $\Phi$  solve for  $w$  and  $z$

Choose  $\beta_2, \Phi$  and  $z$  solve for  $w$  and  $\theta$



# 2-Position Procedure – Dyad 1: Case 1

Choose  $\theta$ ,  $\beta_2$  and  $\Phi$  and solve for  $w$  and  $z$

Let:

$$A = \cos\theta (\cos\beta_2 - 1) - \sin\theta \sin\beta_2$$

$$B = \cos\Phi (\cos\alpha_2 - 1) - \sin\Phi \sin\alpha_2$$

$$C = p_{21} \cos\delta_2$$

$$D = \sin\theta (\cos\beta_2 - 1) + \cos\theta \sin\beta_2$$

$$E = \sin\Phi (\cos\alpha_2 - 1) + \cos\Phi \sin\alpha_2$$

$$F = p_{21} \sin\delta_2$$

Substitute in the equations below:

$$w \cos\theta (\cos\beta_2 - 1) - w \sin\theta \sin\beta_2 + z \cos\Phi (\cos\alpha_2 - 1) - z \sin\Phi \sin\alpha_2 = p_{21} \cos\delta_2$$

$$w \sin\theta (\cos\beta_2 - 1) + w \cos\theta \sin\beta_2 + z \sin\Phi (\cos\alpha_2 - 1) + z \cos\Phi \sin\alpha_2 = p_{21} \sin\delta_2$$

$$A w + B z = C$$

$$D w + E z = F$$

Solve:

$$w = (C E - B F) / (A E - B D)$$

$$z = (A F - C D) / (A E - B D)$$

# 2-Position Procedure – Dyad 1: Case 2

Choose  $\beta_2, \Phi$  and  $z$  solve for  $w$  and  $\theta$

Let:

$$W_{1x} = w \cos\theta$$

$$W_{1y} = w \sin\theta$$

$$Z_{1x} = z \cos\Phi$$

$$Z_{1y} = z \sin\Phi$$

And

$$A = \cos\beta_2 - 1$$

$$B = \sin\beta_2$$

$$C = \cos\alpha_2 - 1$$

$$D = \sin\alpha_2$$

$$E = p_{21} \cos\delta_2$$

$$F = p_{21} \sin\delta_2$$

Substitute in the equations below:

$$w \cos\theta (\cos\beta_2 - 1) - w \sin\theta \sin\beta_2 + z \cos\Phi (\cos\alpha_2 - 1) - z \sin\Phi \sin\alpha_2 = p_{21} \cos\delta_2$$

$$w \sin\theta (\cos\beta_2 - 1) + w \cos\theta \sin\beta_2 + z \sin\Phi (\cos\alpha_2 - 1) + z \cos\Phi \sin\alpha_2 = p_{21} \sin\delta_2$$

$$A W_{1x} - B W_{1y} + C Z_{1x} - D Z_{1y} = E$$

$$A W_{1y} + B W_{1x} + C Z_{1y} + D Z_{1x} = F$$

Solve:

$$W_{1x} = - (A(-CZ_{1x} + DZ_{1y} + E) + B(-CZ_{1y} - DZ_{1x} + F)) / 2A$$

$$W_{1y} = - (A(-CZ_{1y} - DZ_{1x} + F) + B(CZ_{1x} - DZ_{1y} - E)) / 2A$$

# 2-Position Procedure - Dyad 2

2<sup>nd</sup> dyad: US

Define the following variables:

$u$  = length of link2

$\sigma$  = angle of link2 in first position

$\nu_2$  = change in angle of driven link

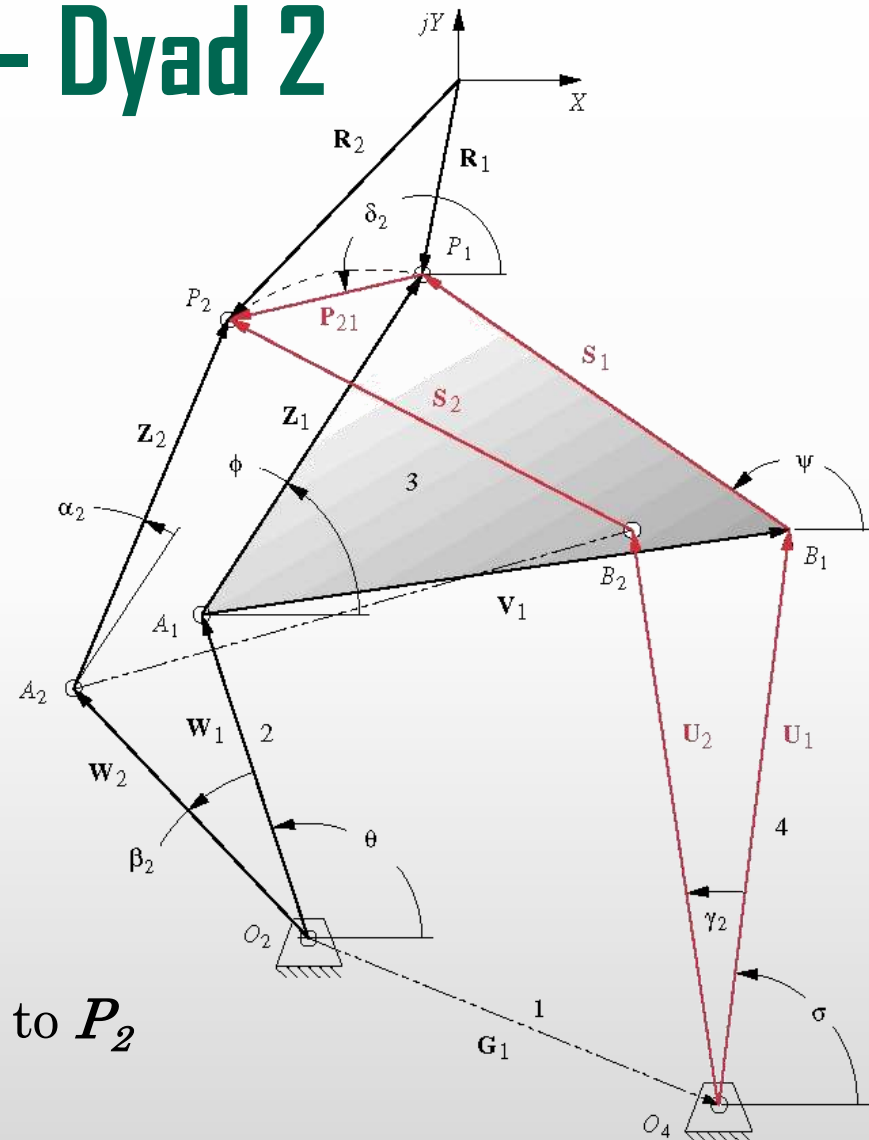
$s$  = distance from point  $B$  to point  $P$

$\Psi$  = orientation angle of link  $s$

$\alpha_2$  = change in orientation of link  $s$

$p_{21}$  = distance from point  $P_1$  to  $P_2$

$\delta_2$  = orientation angle of line from  $P_1$  to  $P_2$





# 2-Position Procedure – Dyad 2

## 2 Equations:

- $u \cos \sigma (\cos \gamma_2 - 1) - u \sin \sigma \sin \gamma_2 + s \cos \psi (\cos \alpha_2 - 1) - s \sin \psi \sin \alpha_2 = p_{21} \cos \delta_2$
- $u \sin \sigma (\cos \gamma_2 - 1) + u \cos \sigma \sin \gamma_2 + s \sin \psi (\cos \alpha_2 - 1) + s \cos \psi \sin \alpha_2 = p_{21} \sin \delta_2$

There are 8 variables in the equations:

3 are given:  $\alpha_2$ ,  $p_{21}$  and  $\delta_2$

Choose 3 variables and solve for 2.

2 Cases to be considered:

Choose  $\sigma$ ,  $\gamma_2$  and  $\psi$  solve for  $u$  and  $s$

Choose  $\gamma_2$ ,  $\psi$  and  $s$  solve for  $u$  and  $\sigma$

# 2-Position Procedure – Dyad 2: Case 1

Choose  $\sigma$ ,  $\gamma_2$  and  $\Psi$  then solve for  $u$  and  $s$

Let:

$$\begin{aligned} A &= \cos\sigma (\cos\gamma_2 - 1) - \sin\sigma \sin\gamma_2 & D &= \sin\sigma (\cos\gamma_2 - 1) + \cos\sigma \sin\gamma_2 \\ B &= \cos\Psi (\cos\alpha_2 - 1) - \sin\Psi \sin\alpha_2 & E &= \sin\Psi (\cos\alpha_2 - 1) + \cos\Psi \sin\alpha_2 \\ C &= p_{21} \cos\delta_2 & F &= p_{21} \sin\delta_2 \end{aligned}$$

Substitute in the equations below:

$$\begin{aligned} u \cos\sigma (\cos\gamma_2 - 1) - u \sin\sigma \sin\gamma_2 + s \cos\Psi (\cos\alpha_2 - 1) - s \sin\Psi \sin\alpha_2 &= p_{21} \cos\delta_2 \\ u \sin\sigma (\cos\gamma_2 - 1) + u \cos\sigma \sin\gamma_2 + s \sin\Psi (\cos\alpha_2 - 1) + s \cos\Psi \sin\alpha_2 &= p_{21} \sin\delta_2 \end{aligned}$$

$$A u + B s = C$$

$$D u + E s = F$$

Solve:

$$u = (C E - B F) / (A E - B D)$$

$$s = (A F - C D) / (A E - B D)$$

# 2-Position Procedure – Dyad 2: Case 2

Choose  $\gamma_2$ ,  $\Psi$  and  $s$  then solve for  $u$  and  $\sigma$

Let:

$$U_{1x} = u \cos\sigma \quad U_{1y} = u \sin\sigma \quad S_{1x} = s \cos\Psi \quad S_{1y} = s \sin\Psi$$

$$\begin{aligned} A &= \cos\gamma_2 - 1 & B &= \sin\gamma_2 & C &= \cos\alpha_2 - 1 \\ D &= \sin\alpha_2 & E &= p_{21} \cos\delta_2 & F &= p_{21} \sin\delta_2 \end{aligned}$$

Substitute in the equations below:

$$\begin{aligned} u \cos\sigma(\cos\gamma_2 - 1) - u \sin\sigma \sin\gamma_2 + s \cos\Psi(\cos\alpha_2 - 1) - s \sin\Psi \sin\alpha_2 &= p_{21} \cos\delta_2 \\ u \sin\sigma(\cos\gamma_2 - 1) + u \cos\sigma \sin\gamma_2 + s \sin\Psi(\cos\alpha_2 - 1) + s \cos\Psi \sin\alpha_2 &= p_{21} \sin\delta_2 \end{aligned}$$

$$AU_{1x} - B U_{1y} + C S_{1x} - D S_{1y} = E$$

$$AU_{1y} + B U_{1x} + C S_{1y} + D S_{1x} = F$$

Solve:

$$U_{1x} = - (A(-CS_{1x} + DS_{1y} + E) + B(-CS_{1y} - DS_{1x} + F)) / 2A$$

$$U_{1y} = - (A(-CS_{1y} - DS_{1x} + F) + B(CS_{1x} - DS_{1y} - E)) / 2A$$

# 2-Position Procedure

## Solution:

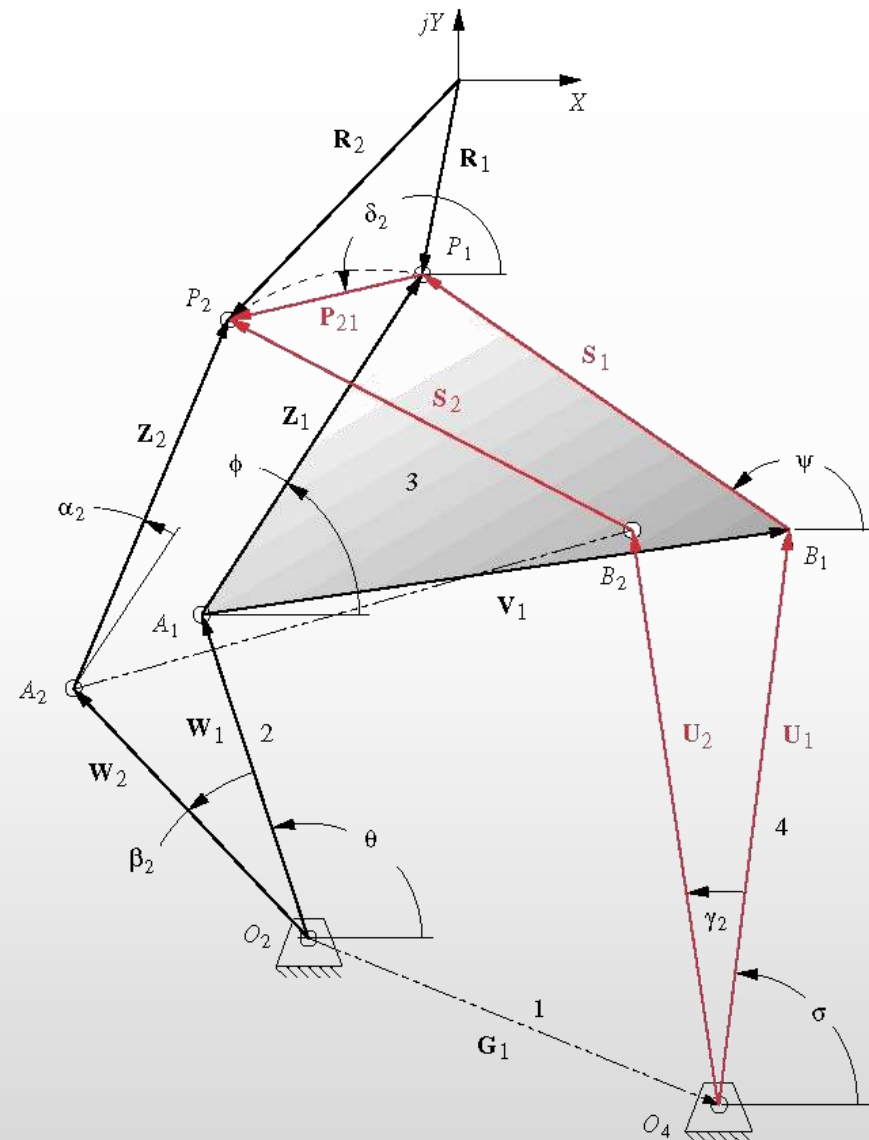
Solve for 1<sup>st</sup> dyad: WZ

Solve for 2<sup>nd</sup> dyad: US

## Use geometry to solve other details

- Position of the pivots ( $O_1$  and  $O_2$ )
- Length of Link 1

(analytical:  $\mathbf{G}_1 = \mathbf{W}_1 + \mathbf{V}_1 - \mathbf{U}_1$ , With  $\mathbf{V}_1 = \mathbf{Z}_1 - \mathbf{S}_1$ )



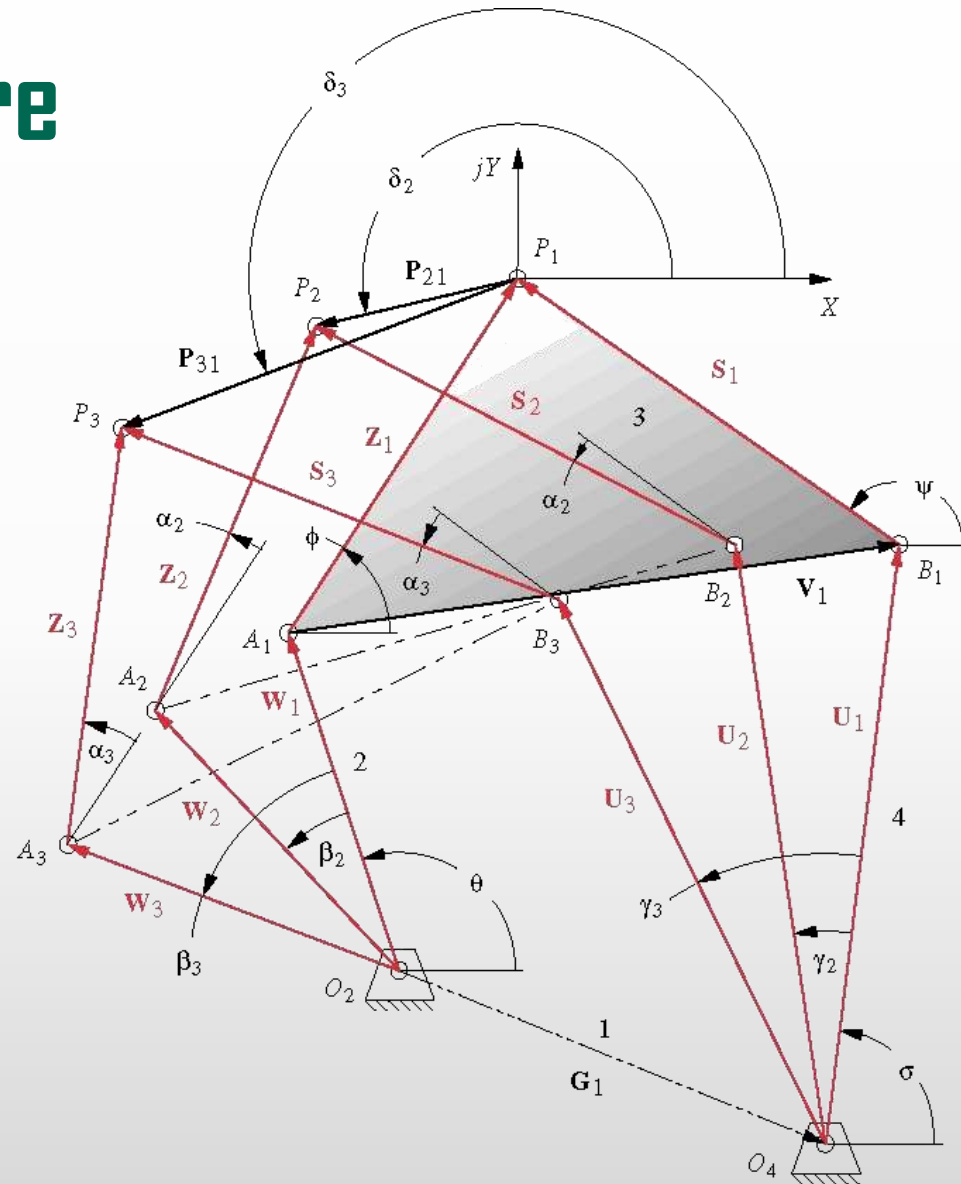


# 3-Position Procedure

Use the same used for 2-position.  
You will have 4 dyads instead of 2

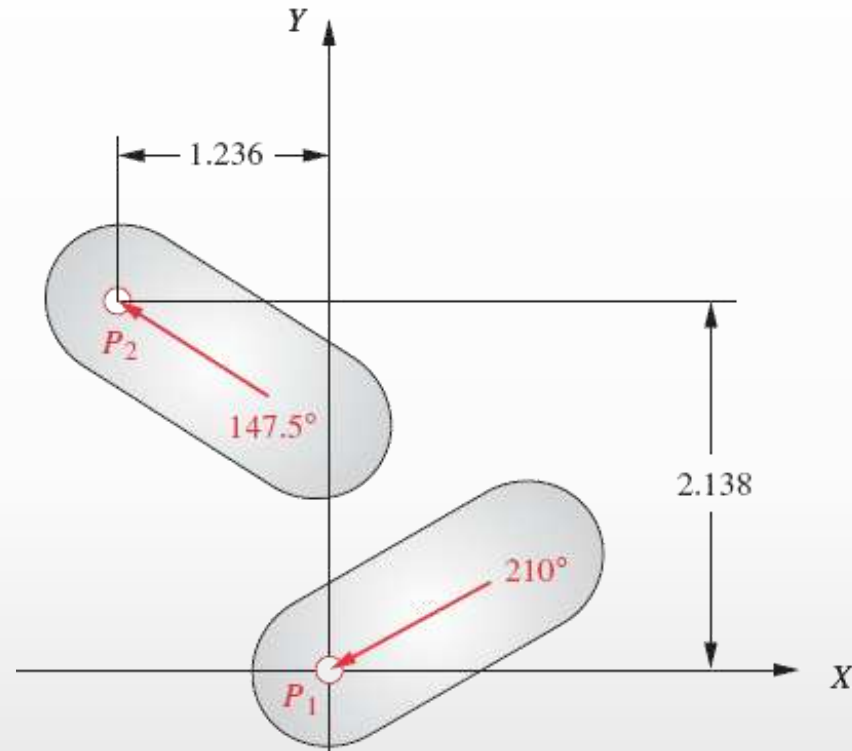
## Solution:

Design of Machinery 5th Edition  
Norton p.223-228



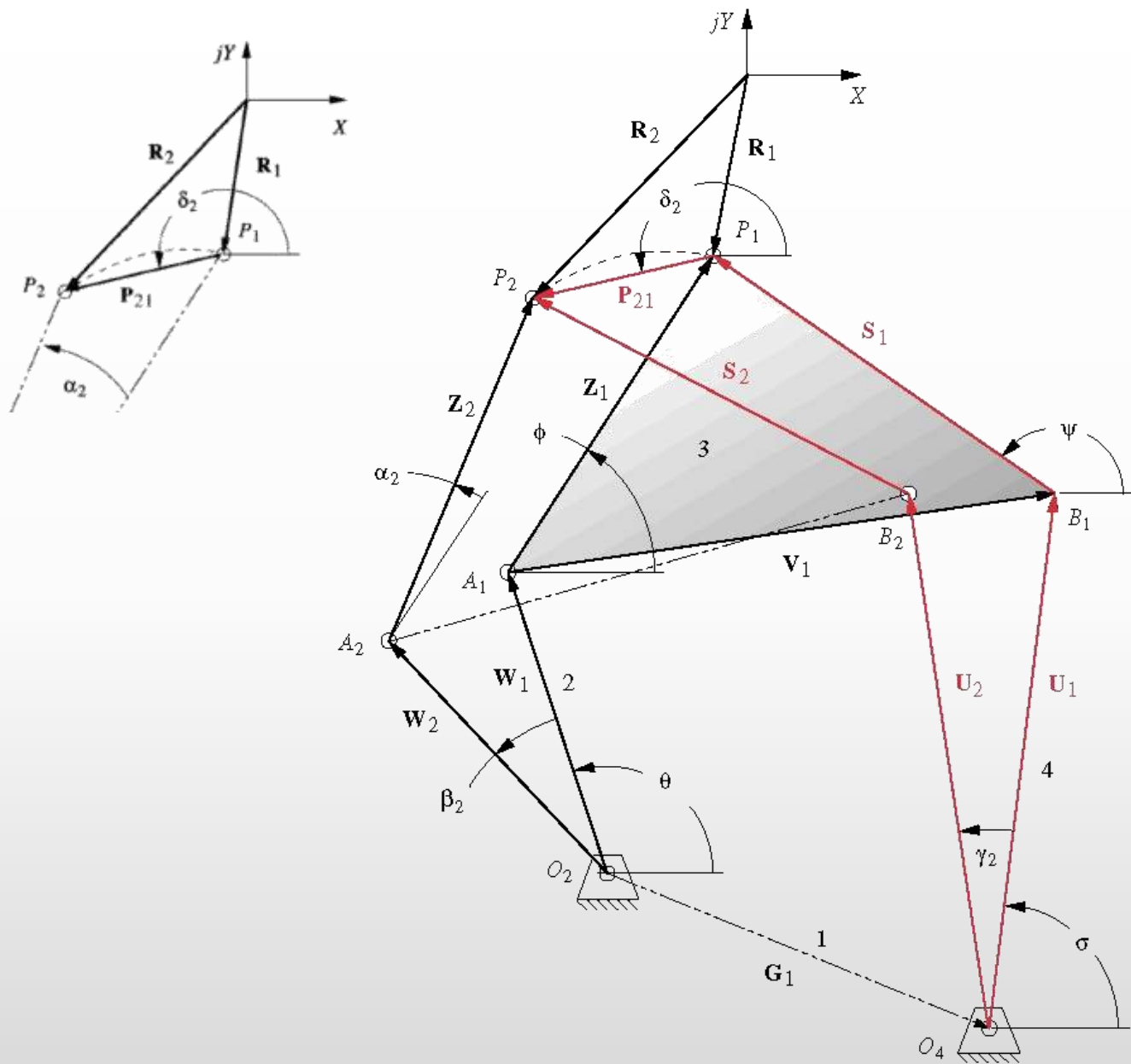
# Problem: 5-8 p.255

- Design a linkage to carry the body in the figure below through the two positions  $P_1$  and  $P_2$  at the angles shown in the figure.
- Use analytical synthesis without regard for the fixed pivots.

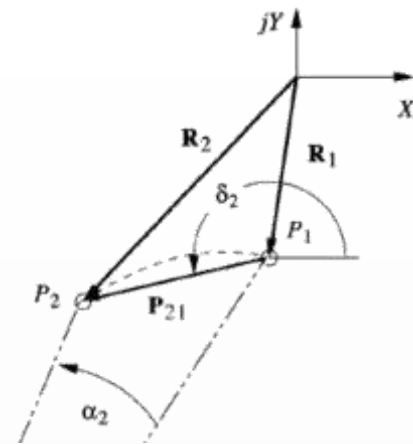


$$1^{\text{st}} \text{ Dyad} \quad z = 1.075, \phi = 204.4^{\circ}, \beta_2 = -27^{\circ}$$

$$2^{\text{nd}} \text{ Dyad} \quad s = 1.24, \psi = 74^{\circ}, \gamma_2 = -40^{\circ}$$



# Solution:



1. Solve the problem using case 2 and the previously generated equations.

2. Define the position vectors  $\mathbf{R}_1$  and  $\mathbf{R}_2$  and the vector  $\mathbf{P}_{21}$  using Figure 5-1 and equation 5.1.

$$R1 := \begin{pmatrix} P_{1x} \\ P_{1y} \end{pmatrix} \quad R2 := \begin{pmatrix} P_{2x} \\ P_{2y} \end{pmatrix} \quad \begin{pmatrix} P_{21x} \\ P_{21y} \end{pmatrix} := R2 - R1 \quad P_{21x} = -1.236$$

$$P_{21y} = 2.138$$

$$p_{21} := \sqrt{P_{21x}^2 + P_{21y}^2}$$

$$p_{21} = 2.470$$

3. From the trigonometric relationships given in Figure 5-1, determine  $\alpha_2$  and  $\delta_2$ .

$$\alpha_2 := \theta_{P2} - \theta_{P1}$$

$$\alpha_2 = -62.500 \text{ deg}$$

$$\delta_2 := \text{atan2}(P_{21x}, P_{21y})$$

$$\delta_2 = 120.033 \text{ deg}$$

# Solution:

4. Solve for the WZ dyad using equations 5.8.

$$Z_{lx} := z \cdot \cos(\phi) \quad Z_{lx} = -0.979 \quad Z_{ly} := z \cdot \sin(\phi) \quad Z_{ly} = -0.444$$

$$A := \cos(\beta_2) - 1 \quad A = -0.109 \quad D := \sin(\alpha_2) \quad D = -0.887$$

$$B := \sin(\beta_2) \quad B = -0.454 \quad E := p_{21} \cdot \cos(\delta_2) \quad E = -1.236$$

$$C := \cos(\alpha_2) - 1 \quad C = -0.538 \quad F := p_{21} \cdot \sin(\delta_2) \quad F = 2.138$$

$$W_{lx} := \frac{A \cdot (-C \cdot Z_{lx} + D \cdot Z_{ly} + E) + B \cdot (-C \cdot Z_{ly} - D \cdot Z_{lx} + F)}{-2 \cdot A} \quad W_{lx} = -1.462$$

$$W_{ly} := \frac{A \cdot (-C \cdot Z_{ly} - D \cdot Z_{lx} + F) + B \cdot (C \cdot Z_{lx} - D \cdot Z_{ly} - E)}{-2 \cdot A} \quad W_{ly} = -3.367$$

$$w := \sqrt{W_{lx}^2 + W_{ly}^2} \quad w = 3.670$$

$$\theta := \text{atan2}(W_{lx}, W_{ly}) \quad \theta = 246.528 \text{ deg}$$

# Solution:

5. Solve for the US dyad using equations 5.12.

$$S_{Ix} := s \cdot \cos(\psi) \quad S_{Ix} = 0.342 \quad S_{Iy} := s \cdot \sin(\psi) \quad S_{Iy} = 1.192$$

$$A := \cos(\gamma_2) - 1 \quad A = -0.234 \quad D := \sin(\alpha_2) \quad D = -0.887$$

$$B := \sin(\gamma_2) \quad B = -0.643 \quad E := p_{2I} \cdot \cos(\delta_2) \quad E = -1.236$$

$$C := \cos(\alpha_2) - 1 \quad C = -0.538 \quad F := p_{2I} \cdot \sin(\delta_2) \quad F = 2.138$$

$$U_{Ix} := \frac{A \cdot (-C \cdot S_{Ix} + D \cdot S_{Iy} + E) + B \cdot (-C \cdot S_{Iy} - D \cdot S_{Ix} + F)}{-2 \cdot A} \quad U_{Ix} = -3.180$$

$$U_{Iy} := \frac{A \cdot (-C \cdot S_{Iy} - D \cdot S_{Ix} + F) + B \cdot (C \cdot S_{Ix} - D \cdot S_{Iy} - E)}{-2 \cdot A} \quad U_{Iy} = -4.439$$

$$u := \sqrt{U_{Ix}^2 + U_{Iy}^2} \quad u = 5.461$$

$$\sigma := \text{atan2}(U_{Ix}, U_{Iy}) \quad \sigma = 234.381 \text{ deg}$$

# Solution:

6. Solve for links 3 and 1 using the vector definitions of **V** and **G**.

Link 3:  $V_{Ix} := z \cdot \cos(\phi) - s \cdot \cos(\psi) \quad V_{Ix} = -1.321$

$V_{Iy} := z \cdot \sin(\phi) - s \cdot \sin(\psi) \quad V_{Iy} = -1.636$

$\theta_3 := \text{atan2}(V_{Ix}, V_{Iy}) \quad \theta_3 = 231.086 \text{ deg}$

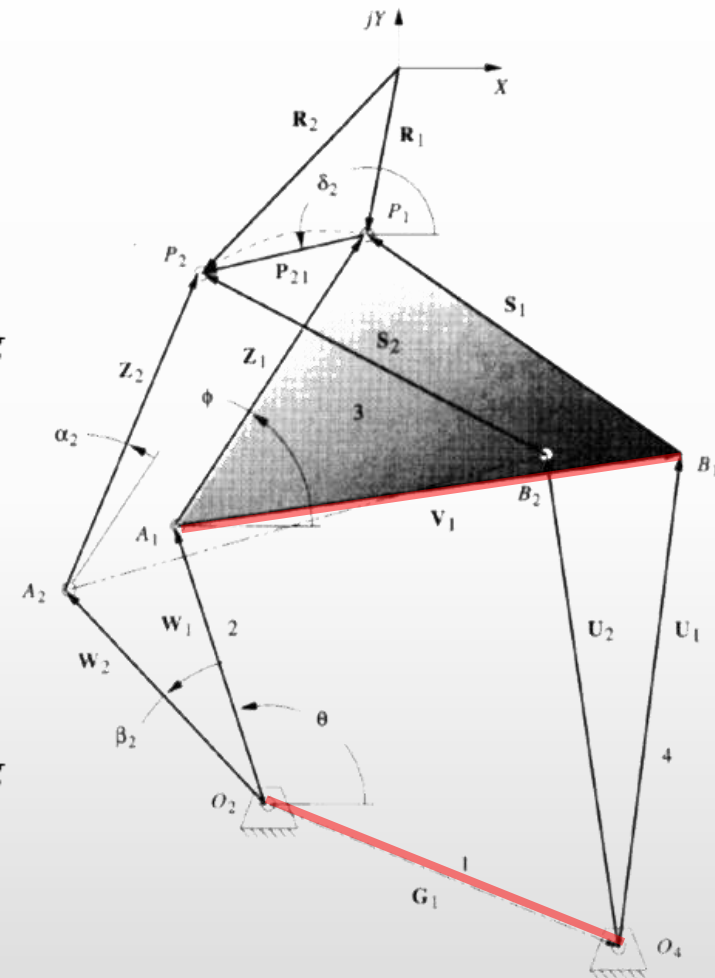
$v := \sqrt{V_{Ix}^2 + V_{Iy}^2} \quad v = 2.103$

Link 1:  $G_{Ix} := w \cdot \cos(\theta) + v \cdot \cos(\theta_3) - u \cdot \cos(\sigma) \quad G_{Ix} = 0.398$

$G_{Iy} := w \cdot \sin(\theta) + v \cdot \sin(\theta_3) - u \cdot \sin(\sigma) \quad G_{Iy} = -0.564$

$\theta_1 := \text{atan2}(G_{Ix}, G_{Iy}) \quad \theta_1 = -54.796 \text{ deg}$

$g := \sqrt{G_{Ix}^2 + G_{Iy}^2} \quad g = 0.690$



# Solution:

7. Determine the initial and final values of the input crank with respect to the vector **G**.

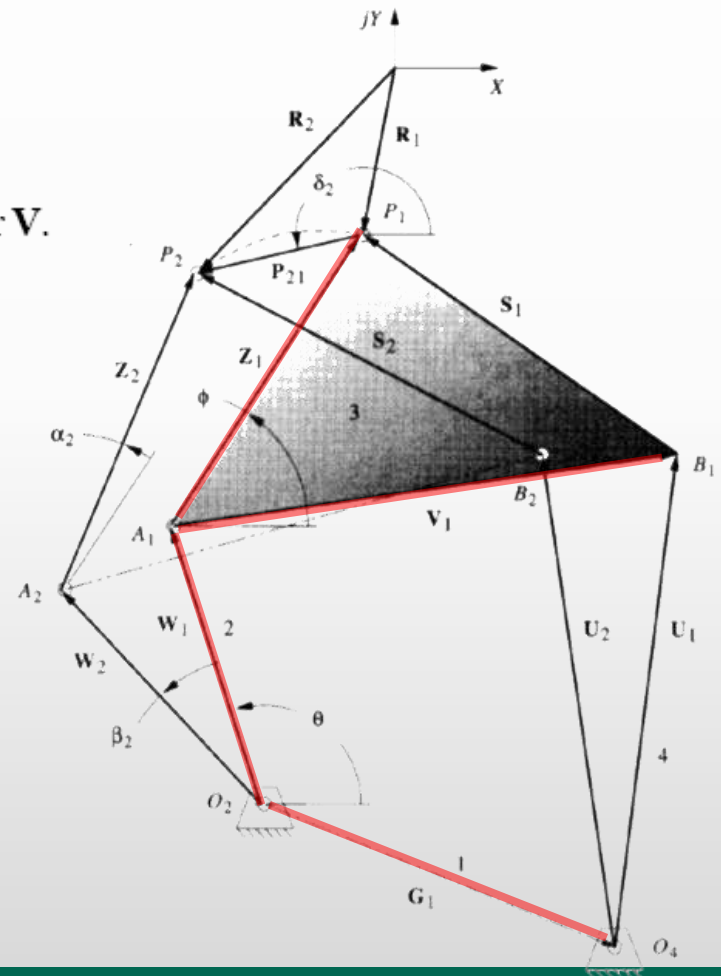
$$\theta_{2i} := \theta - \theta_1 \quad \theta_{2i} = 301.323 \text{ deg}$$

$$\theta_{2f} := \theta_{2i} + \beta_2 \quad \theta_{2f} = 274.323 \text{ deg}$$

8. Define the coupler point with respect to point **A** and the vector **V**.

$$r_p := z \quad \delta_p := \phi - \theta_3$$

$$r_p = 1.075 \quad \delta_p = -26.686 \text{ deg}$$





# Solution:

9. Locate the fixed pivots in the global frame using the vector definitions

$$\rho_1 := \text{atan2}(P_{1x}, P_{1y})$$

$$\rho_1 = 180.000 \text{ deg}$$

$$R_I := \sqrt{P_{1x}^2 + P_{1y}^2}$$

$$R_I = 0.000$$

$$O_{2x} := R_I \cos(\rho_1) - z \cos(\phi) - w \cos(\theta)$$

$$O_{2x} = 2.441$$

$$O_{2y} := R_I \sin(\rho_1) - z \sin(\phi) - w \sin(\theta)$$

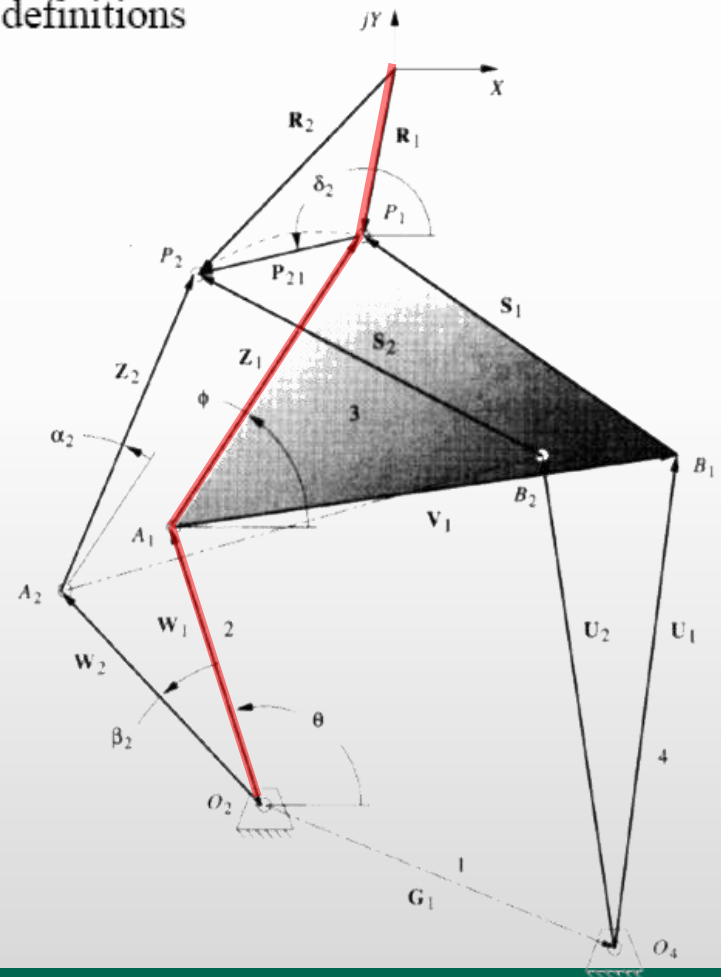
$$O_{2y} = 3.811$$

$$O_{4x} := R_I \cos(\rho_1) - s \cos(\psi) - u \cos(\sigma)$$

$$O_{4x} = 2.838$$

$$O_{4y} := R_I \sin(\rho_1) - s \sin(\psi) - u \sin(\sigma)$$

$$O_{4y} = 3.247$$



# Solution:

10. Determine the rotation angle of the fourbar frame with respect to the global frame (angle from the global X axis to the line  $O_2O_4$ ).

$$\theta_{rot} := \text{atan2}[(O_{4x} - O_{2x}), (O_{4y} - O_{2y})] \quad \theta_{rot} = -54.796 \text{ deg}$$

11. Determine the Grashof condition.

$$\text{Condition}(a, b, c, d) := \begin{cases} S \leftarrow \min(a, b, c, d) \\ L \leftarrow \max(a, b, c, d) \\ SL \leftarrow S + L \\ PQ \leftarrow a + b + c + d - SL \\ \text{return "Grashof" if } SL < PQ \\ \text{return "Special Grashof" if } SL = PQ \\ \text{return "non-Grashof" otherwise} \end{cases}$$

# Solution:

## 12. DESIGN SUMMARY

Link 2:	$w = 3.670$	$\theta = 246.528 \text{ deg}$
Link 3:	$v = 2.103$	$\theta_3 = 231.086 \text{ deg}$
Link 4:	$u = 5.461$	$\sigma = 234.381 \text{ deg}$
Link 1:	$g = 0.690$	$\theta_1 = -54.796 \text{ deg}$
Coupler:	$r_p = 1.075$	$\delta_p = -26.686 \text{ deg}$
Crank angles:		
	$\theta_{2i} = 301.323 \text{ deg}$	
	$\theta_{2f} = 274.323 \text{ deg}$	

# Solution:

13. Draw the linkage, using the link lengths, fixed pivot positions, and angles above, to verify the design.

